



STELLENBOSCH MUNICIPALITY

**WATER DISTRIBUTION SYSTEM -
PIPE REPLACEMENT STUDY**

June 2019



**WATER DISTRIBUTION SYSTEM -
PIPE REPLACEMENT STUDY**

June 2019

TABLE OF CONTENTS

	<i>Pp</i>
1. INTRODUCTION	1
1.1 BRIEF.....	1
1.2 SCOPE OF THE REPORT	1
1.3 DISCLAIMER	1
2. METHODOLOGY.....	2
2.1 INTRODUCTION	2
2.2 FACTORS CONTRIBUTING TO LIKELIHOOD OF FAILURE	4
2.2.1 <i>Nominal diameter</i>	4
2.2.2 <i>Reserve water pressure ratio</i>	4
2.2.3 <i>Catalogue remaining useful life</i>	5
2.2.4 <i>Master plan item</i>	6
2.2.5 <i>Assessed condition</i>	6
2.2.6 <i>Failure frequency</i>	7
2.2.7 <i>Leakage volume</i>	8
2.2.8 <i>Undesired material</i>	8
2.2.9 <i>Geology</i>	9
2.3 FACTORS CONTRIBUTING TO CONSEQUENCE OF FAILURE.....	10
2.3.1 <i>High cost to consumer due to high water pressure</i>	10
2.3.2 <i>High cost to consumer due to flow</i>	10
2.3.3 <i>High repair cost</i>	11
2.3.4 <i>Flooding due to geography</i>	11
2.3.5 <i>Strategic location</i>	12
2.3.6 <i>Network redundancy</i>	12
2.3.7 <i>Pavement management system (PMS)</i>	13
2.4 SOFTWARE MODEL.....	13
3. DISCUSSION OF RESULTS.....	15
4. RECOMMENDATION	16
5. CONCLUSION	17
APPENDIX – FIGURES AND TABLES	18

LIST OF FIGURES*Pp*

Figure 1: Graphical result where PRP is also influenced by slope analysis (on aerial image).....	14
Figure 2: Graphical result – detail view.....	14
Figure SRW 1(a): Pipe replacement potential for Stellenbosch	21
Figure SRW 1(b): Pipe replacement potential for Dwarsrivier	22
Figure SRW 1(c): Pipe replacement potential for Klapmuts	23
Figure SRW 1(d): Pipe replacement potential for Franschhoek	24
Figure SRW 1(e): Pipe replacement potential for Raithby.....	25
Figure SRW 2: Pipe length weighted average PRP per town (Percentage).....	26

LIST OF TABLES*Pp*

Table SRW 1: Top 112 pipes in Stellenbosch to be replaced based on PRP	19
Table SRW 2: Processed pipe failure record	20

LIST OF ABBREVIATIONS & ACRONYMS

AC/FC	-	Fibre reinforced cement
CBD	-	Central business district
CF	-	Consequence of failure
CI	-	Cast iron
CO	-	Copper
DI	-	Ductile iron
FF	-	Failure frequency
GIS	-	Geographic information system
GLS	-	GLS consulting engineers
GRP	-	Glass reinforced plastic
HDPE	-	High density polyethylene
kℓ	-	Kilolitre
kℓ/d	-	Kilolitre/day
km	-	Kilometre
kW	-	Kilowatt
kWh	-	Kilowatt-hour
ℓ	-	Litre
ℓ/day/UE	-	Litre/day/unit erf
ℓ/h/connection	-	Litre/hour/connection
ℓ/min	-	Litre/minute
ℓ/s	-	Litre/second
LDPE	-	Low density polyethylene
LF	-	Likelihood of failure
m	-	Metre
Mℓ	-	Megalitre
mm	-	Millimetre
MP	-	Master plan
mPVC	-	Modified polyvinyl chloride
PMS	-	Pavement management system
POS	-	Public open space
PRP	-	Pipe replacement potential
PVC	-	Polyvinyl chloride
RUL	-	Remaining useful life
uPVC	-	Unplasticized polyvinyl chloride
WADISO	-	Water distribution system optimization program (software)

1. INTRODUCTION

1.1 BRIEF

GLS Consulting (GLS) was appointed to perform a pipe replacement prioritisation study for the entire water distribution system of the Stellenbosch Municipality. This study was documented in a report dated March 2012. GLS was subsequently appointed to update the 2012 study.

The project entails the verification of system data, compilation of a computer model for the pipe replacement network, calibration of the computer model, work shopping of the relevant factors and weights applied in the analysis and performing the analysis.

1.2 SCOPE OF THE REPORT

This report addresses the prioritisation of replacing water pipes within the Stellenbosch Municipality, comprising the towns of Stellenbosch, Dwarsrivier, Klapmuts, Franschhoek and Raithby.

1.3 DISCLAIMER

The investigation has been performed and this report has been compiled based on the information made available to GLS. All efforts, within budget constraints, have been made during the gathering of information to ensure the highest degree of data integrity. The information supplied to GLS by the Stellenbosch Municipality and other consultants at the outset of this pipe replacement plan is assumed to be the most accurate representation of the existing system up to date hereof.

All recommendations pertaining to identifying pipes for replacement should be regarded as an initial best assumption, but the knowledge which the field staff may have regarding the condition of the various pipes should also be taken into account by the client in order to verify the pipe replacement priority before commencing any upgrading projects.

Subsequent to the completion of the data capturing the layout plans, including the relevant attributes, were handed back to the Municipality so that the information could be verified by the client. GLS can therefore not be held accountable for inaccurate information received pertaining to the components of the existing system.

2. METHODOLOGY

2.1 INTRODUCTION

The pipe replacement potential (PRP) for any one pipe in the water distribution model is assessed by combining two critical indices – the likelihood of failure (LF) and consequence of failure (CF). Various independent factors contribute to each of these indices.

For the LF the following independent factors have been identified pertaining to each pipe which will be discussed in more detail in paragraph 2.2 below.

1. Nominal diameter.
2. Reserve water pressure ratio.
3. Catalogue remaining useful life.
4. Master plan item
5. Assessed condition.
6. Failure frequency.
7. Leakage volume.
8. Undesired material.
9. Geology.

For the CF the following independent factors have been identified pertaining to each pipe which will be discussed in more detail in paragraph 2.3 below.

1. High cost to consumer due to high water pressure.
2. High cost to consumer due to flow.
3. High repair cost.
4. Flooding due to geography.
5. Strategic location.
6. Network redundancy.
7. Pavement management system alignment.

The various contributing factors are assessed for each pipe by allocating a rating value (0 to 5) to each factor. The contributing factors are then totalled using various respective weights and normalized to give a total LF or CF index in the range of 1 to 5 respectively. A LF % and CF % is also calculated with the ranked LF and CF values respectively.

An initial weight distribution for LF was adopted for Stellenbosch, but it was refined during workshop sessions with officials of the Municipality and amended as follows:

Likelihood of Failure Property	Score out of 10	Weight (%)
Nominal diameter (mm)	5.4	16
Reserve water pressure ratio	2.6	8
Catalogue remaining useful life (yr)	4.6	14
Master plan item*	0.0	0
Assessed condition	5.0	15
Failure frequency (breaks/km/yr)	8.9	26
Leakage volume (l/min/km)*	0.0	0
Undesired material	7.1	21
Geology *	0.0	0
TOTAL		100.0

* Data not available for or relevant to Stellenbosch Municipality

Likewise an initial weight distribution for CF was adopted for Stellenbosch, which was also refined during the workshop session and amended as follows:

Consequence of failure Property	Score out of 10	Weight (%)
High cost to consumer due to high water pressure	2.2	8
High cost to consumer due to flow	2.2	8
High repair cost*	3.5	12
Flooding due to geography*	7.3	26
Strategic location	6.0	21
Network redundancy	7.3	26
Pavement management system*	0.0	0
TOTAL		100.0

* Data not available for or relevant to Stellenbosch Municipality

The source data could have a granularity larger than that of one pipe (e.g. Geology could be defined for a whole area covering a selection of pipes). In this case contributing factors are assessed by spreading the overall value onto the entities of smallest granularity, i.e. over the individual modelled pipes.

The total PRP is then calculated for each pipe as an index

$$\text{PRP} = \text{LF} \times \text{CF} \text{ (in the range of 1 to 25)}$$

By calculating the product of the two indices the compound risk is assessed. Only if a pipe has a high index for likelihood of failure and a high risk for consequence of failure will a high potential for replacement result. In addition the expected replacement cost for every pipe is calculated. The table of pipes in the model can then be sorted in order of decreasing PRP and a ranking PRP% from 100% to 0% is also displayed. The pipes with the highest replacement potential can then be visualized graphically and the associated total replacement cost determined.

The PRP can then be aggregated in various ways to provide a weighted average, maximum or minimum for various collections, such as per

- Region (Township, suburb or neighbourhood)
- System (Reservoir zone or other subsystem)

2.2 FACTORS CONTRIBUTING TO LIKELIHOOD OF FAILURE

The procedure followed to determine each of the factors contributing to the LF is outlined below:

2.2.1 Nominal diameter

The Wadiso model contains a user definable field which contains the nominal pipe diameter. The basic assumption here is the larger the pipe diameter the less likely pipe failures will result. This is a primary factor which should ideally only be used when better information on the likelihood of failure is not available. The following classification index was adopted to rate this factor:

Property	Criteria (\leq)	Rating (0..5)
Nominal diameter (mm)	50	5
Nominal diameter (mm)	75	4
Nominal diameter (mm)	110	3
Nominal diameter (mm)	160	2
Nominal diameter (mm)	250	1
Nominal diameter (mm)	400	0.5
Nominal diameter (mm)	>400	0.1

It can be seen that very small diameters are severely penalized (high rating). Diameters above 400 mm are regarded as less likely to fail and are not penalized. A value of 0.1 is adopted here instead of 0 to ensure fewer pipes end up with identical PRP values and corresponding equal PRP%.

2.2.2 Reserve water pressure ratio

The concept of a reserve pressure ratio is introduced. Every pipe in the model can have the property [Pressure rating (kPa)] which expresses the maximum allowable service pressure of the pipe. This value is converted to units of metre (m) water pressure.

The highest pressures in a pipe network are usually experienced during static (low flow or night time) conditions. The result of the static analysis is presented at the nodes of the model. Every pipe has an upstream and a downstream node for which the static pressure is available from the Wadiso result variables. The [Pipe average static pressure (m)] is then determined by averaging the nodal static pressures, i.e. [(US SHead+DS SHead)/2]. Should this value be negative, a zero value is assumed. The reserve pressure ratio is then defined as

$$[\text{Pipe average static pressure (m)}] / [\text{Pressure rating (m)}]$$

Should the pressure rating be zero for some reason (invalid data) then a zero reserve pressure ratio is assumed. A reserve pressure rating of 1.0 indicates that the pipe has no reserve capacity with regards to pressure and a rating of bigger than 1.0 indicates over stressing the pipe risking severe pipe rupture.

Should the pressure rating not be available for the pipes in the model, a suitable default value should be entered, such as 90 m (or for example 899 kPa to flag the

value as unknown). This will have the side effect of only evaluating the model based on average static pressure. The following classification index was adopted to rate this factor:

Property	Criteria (<=)	Rating (0..5)
Reserve pressure ratio	0	0.1
Reserve pressure ratio	0.25	1
Reserve pressure ratio	0.50	2
Reserve pressure ratio	0.75	3
Reserve pressure ratio	1	4
Reserve pressure ratio	>1	5

It can be seen that the rating increases as the reserve pressure increases to unity.

2.2.3 Catalogue remaining useful life

For every pipe in the model the remaining useful life (RUL) can be determined. The Wadiso model should contain the material for every pipe in the model. For every material a standard life is assumed for a pipe of that material, as outlined typically in the table below:

Property	Criteria	Life (yr)
Pipe material life	Fibre reinforced cement (FC or AC)	40
Pipe material life	(undefined)	40
Pipe material life	Modified polyvinyl chloride (mPVC)*	50
Pipe material life	Glass reinforced plastic (GRP)*	60
Pipe material life	Unplasticized polyvinyl chloride (uPVC)	60
Pipe material life	High density polyethylene (HDPE)	80
Pipe material life	Low density polyethylene (LDPE)*	80
Pipe material life	"Polycop" plastic piping (POLYCOP)	80
Pipe material life	Copper (CO)	60
Pipe material life	Steel (STEEL)	80
Pipe material life	Cast iron (CI)	100
Pipe material life	Ductile iron (DI)*	100

* Data not available for or relevant to Stellenbosch Municipality

For pipes of unknown material (i.e. blank) an average life of 40 years is assumed. For every pipe in the Wadiso model, the year of installation of the pipe [AM*_year] should be available. This can often be obtained from asset register databases. The RUL for any pipe is then calculated as:

$$[\text{Standard life expectancy based on material}] - ([\text{Current year}] - [\text{AM year}])$$

Should the year of installation be unknown, the average age is calculated from all known installations and fourty years was used for Stellenbosch Municipality.

The following classification index was adopted to rate this factor:

Property	Criteria (<=)	Rating (0..5)
Remaining useful life (yr)	0	5
Remaining useful life (yr)	10	4
Remaining useful life (yr)	20	3
Remaining useful life (yr)	30	2
Remaining useful life (yr)	50	1
Remaining useful life (yr)	>50	0.1

It can be seen that the rating decreases as the RUL increases.

2.2.4 Master plan item

As part of the master plan (MP) of a water distribution network, pipes in the present model are identified, which should be upgraded by either replacement or parallel reinforcement. This provides an independent assessment by an engineer of those pipes that should be replaced in the water network based on the hydraulic capacity of the pipe.

The rationale of the MP item concept is that if a pipe has to be replaced due to insufficient hydraulic capacity, the replacement of this pipe can be brought forward if the other criteria indicate an increased likelihood of failure.

Usually only the future model (which includes schematic pipes for future extensions to the model) is provided to the client, with all the MP items identified. By spatially mapping the pipes identified with the MP prefix in the [MP type] field to pipes existing in the present model, the present model is augmented with the required information.

The following classification index was adopted to rate this factor:

Property	Criteria	Rating (0..5)
MP item type	(undefined)	3
MP item type	MP*	5

* Data not available for or relevant to Stellenbosch Municipality

2.2.5 Assessed condition

Pipes of poor quality or those known likely to fail can be identified. Care must however be taken not to base the assessed condition on another factor already considered such as pipe age or RUL. Data regarding the condition of the pipes in Stellenbosch Municipality was unavailable and this factor was not included. It is suggested the following classification index be adopted to rate this factor. A two character string is proposed (with meaning in brackets).

Property	Criteria	Rating (0..5)
AM condition	VG (Very good)	1
AM condition	G (Good)	2
AM condition	(undefined)	3
AM condition	F (Fair)	3
AM condition	P (Poor)	4
AM condition	VP (Very poor)	5

2.2.6 Failure frequency

Logged pipe failure is an important source of information to identify where pipe failures are likely to occur in future. Although a pipe section of the failed pipe would have been replaced by a new pipe, the underlying reason for failure might not have been resolved and future failures are likely to occur again in adjacent sections until a pipe replacement of the total street block or area of pipes has been done.

Typically a report containing information on the location, closest stand number (in some cases), street address (in some cases) and dates of pipe burst recording and repair is available. In Stellenbosch Municipality 3 121 incidents were captured for the period January 2001 to January 2012 and 1 286 incidents were captured for the period January 2013 to February 2018. This information was made available by Stellenbosch Municipality in hard copy and spread sheet format.

Then a process of geo-coding was followed to assign a latitude & longitude coordinate to the location of every incident as accurately as possible. This included using a cadastral CAD layer with stand numbers, a CAD drawing containing street names and the use of the latest street mapping software to geo-reference street number addresses. A total of 926 (86%) of the incident location could be successfully geo-referenced. The data was then converted from spreadsheet to point shape geographical information system (GIS) files with the incident address, repair completion date and completion year as attributes. Typically where the street number (or stand number) was not available, but only the road name, a location closest to middle of the street length was identified. For streets of short distance this is acceptable but for long streets this does introduce an approximation to the exact failure location. A total of 574 out of the 926 geo-referenced locations (62%) were thus approximate. It was however decided to use this data albeit that it was not very accurately located.

The relatively low percentage of breaks that could not be successfully geo-references is due to the lack of addresses or co-ordinates in the original data set.

See Table SRW 2 in Appendix for the final dataset used.

The pipe data model was then extended with fields to store the number of pipe failures per year for the surveyed years (2011 - 2018, but considering that the failure record is not the same for all areas) as well as the average annual number of pipe failures per length of modelled pipe. Results vary from a maximum of 28,6 incidents per year per km of modelled pipe to zero incidents per pipe.

By doing a spatial correlation between point shape file and the closest modelled pipe (using a custom function written to count the number of failures allotted to a pipe for each year up to a distance of 100 m away from any pipe and then divide the sum by

the total length of the modelled pipe in km), the above fields in the pipe data model were updated. Typically the modelled pipe comprises many pipe sections and thus the adjacent sections more likely to fail than the replaced one, will also be identified. This resulted in 647 pipes allocated with a non-zero failure frequency (FF).

It was decided to exclude failure counts where the spatially correlated pipe was replaced within the same year or after the failure was recorded. This assumes that the reason for the failure was related to the old pipe and that future failures are now unlikely to occur at that pipe. This resulted in 554 pipes allocated with a non-zero FF.

The following classification index was adopted after doing a frequency distribution on the data, to rate this factor. A value of 3 failures per year per km of modelled pipe was taken as approximately the 85 percentile and limit for the last open category.

Property	Criteria (<=) (Failures/yr/km)	Rating (0..5)
Failure frequency	0	0.1
Failure frequency	1	0.5
Failure frequency	2	1
Failure frequency	3	3
Failure frequency	4	4
Failure frequency	>4	5

2.2.7 Leakage volume

The historic bulk delivery of water into a zone can be measured by a zone meter. The end-user consumption of the water provided to the zone can be obtained from treasury water sales records. Provided zone meters are installed covering a number of smaller zones a water balance analysis can be performed for the smaller zones. Then by performing a zone to modelled pipe spatial correlation the pipe data model can be extended to include a [Leakage volume] field.

In Stellenbosch typically only a few bulk meters exist and the water balance and resulting calculation of leakage volume per pipe does not assist in identifying pipes to be prioritized for replacement. In the case of Stellenbosch Municipality this index has therefore been ignored.

2.2.8 Undesired material

Pipe material plays a large role in pipe replacement prioritisation. With technology development, improved and cheaper materials are discovered which expose older materials unwanted characteristics. These unwanted materials need to be replaced.

The Wadiso model should contain the material for every pipe in the model. Each material is outlined in the table below:

Property	Criteria (<=) (Failures/yr/km)	Rating (0..5)
Undesired material	Ductile Iron (DI)	1
Undesired material	HDPE	1
Undesired material	STEEL	1
Undesired material	LDPE*	2
Undesired material	uPVC	2
Undesired material	(undefined)	3
Undesired material	CI	3
Undesired material	POLYCOP	4
Undesired material	AC	5
Undesired material	COPPER	5

* Data not available for or relevant to Stellenbosch Municipality

2.2.9 Geology

The geology in the area surrounding installed pipes can play a role in pipe replacement prioritisation. Where pipes have been installed in clay or dolomite areas a higher replacement likelihood is predicted especially in combination with non-flexible type pipe materials. In the case of Stellenbosch Municipality no information on expansive clays were initially available and to our knowledge no dolomite is present in this area and therefore this factor was also ignored in the analysis.

The following classification index can be used to rate this factor where two degrees of dolomite are supported.

Property	Criteria	Rating (0..5)
Geology	NO DOLOMITE or CLAY	0.1
Geology	(undefined)	2.5
Geology	EXP. CLAY	3
Geology	DOLOMITE 1	4
Geology	DOLOMITE 2	5

2.3 FACTORS CONTRIBUTING TO CONSEQUENCE OF FAILURE

The procedure followed to determine each of the factors contributing to the CF is outlined below:

2.3.1 High cost to consumer due to high water pressure

The Wadiso model data contains the balanced results after a steady-state analysis for the present operational average day demand scenario. This scenario models the situation in the pipe network expected on the average day of the year. During a pipe failure damage due to flooding can occur. The higher the water pressure in the pipe network the higher the potential for high damage cost to the consumer.

The field [AvgHead (m)] is available in the pipe data model to assess this factor. The following classification index was adopted to rate this factor:

Property	Criteria (<=)	Rating (0..5)
Consumer loss head (m)	0	0.1
Consumer loss head (m)	25	1
Consumer loss head (m)	50	2
Consumer loss head (m)	75	3
Consumer loss head (m)	100	4
Consumer loss head (m)	>100	5

2.3.2 High cost to consumer due to flow

The Wadiso model data contains the balanced results after a steady-state analysis for the present operational average day demand scenario. This scenario models the situation in the pipe network expected on the average day of the year. During a pipe failure damage due to flooding can occur. The higher the flow in the pipe network the higher the potential for high damage cost to the consumer. This can be unrelated to the pressure in the network at the point.

If a pipe is delivering water to consumers, i.e. not only feeding storage facilities such as reservoirs, then the flow in the pipe is directly proportional to the demand of the connected consumer(s). The potential cost of claims to the water service provider from the consumer due to the non-supply of water as a result of a pipe failure is again directly proportional to the amount of flow in the pipe.

The field [Flow (m)] is available in the pipe data model to assess this factor. The following classification index was adopted to rate this factor:

Property	Criteria (<=)	Rating (0..5)
Consumer loss flow (l/s)	0	0.1
Consumer loss flow (l/s)	5	1
Consumer loss flow (l/s)	10	2
Consumer loss flow (l/s)	20	3
Consumer loss flow (l/s)	50	4
Consumer loss flow (l/s)	>50	5

2.3.3 High repair cost

The Wadiso model data contains data that classifies the type of pipe in the present model with respect to the excavation type in case of repair. The field [Cost_FN] mainly identifies where pipes are located in a road reserve (default) or under a road. Alternatively pipes located in a public open space (POS) can also be identified. Should this information not be available initially all pipes crossing or under roads can be identified graphically by overlaying the model on the cadastral and/or aerial imagery. Due to the uncertainty re the exact position of pipes this has not been performed for the Stellenbosch Municipality.

The following classification index was adopted to rate this factor:

Property	Criteria	Rating (0..5)
Repair cost	Public open space*	1.0
Repair cost	Road reserve/undefined*	3
Repair cost	Under road*	5

* Data not available for or relevant to Stellenbosch Municipality

2.3.4 Flooding due to geography

In order to quantify the likelihood of flooding due to the geography with emphasis on the cross slope of roads, a graphical interactive slope analysis is performed to establish whether a pipe is installed on the higher or lower side of a road. Should a pipe be located in a road reserve clearly on the higher side of a road, it is expected that should the pipe fail, water will collect mostly in the stormwater system of the road and thus not flood the properties on the lower side of the road. However, should the pipe be located in a road reserve on the lower side of the road, flooding of the properties on the lower side is imminent.

In order to identify the pipes which run parallel to height contours, only those pipes are highlighted initially which do not have a steep absolute slope over their length. Then with the contours overlaid, only the subset of pipes which are located in areas of steeper contours (typically with more than 10% fall over the width of the road) have been identified.

Then only the pipes on the lower side of the road (more critical) have been identified and the undefined value adopted for all other pipes.

The following classification index was adopted to rate this factor:

Property	Criteria	Rating (0..5)
Side of road	(undefined)*	3
Side of road	Lower*	5
Side of road	Midblock	5

* Data not available for or relevant to Stellenbosch Municipality

2.3.5 Strategic location

In order to accommodate the effect of strategic location with emphasis on high density industrial areas, hospitals or central business district (CBD) areas, a classification index is adopted for this factor:

Property	Criteria	Rating (0..5)
Strategic location	(undefined)	3
Strategic location	Industrial	4
Strategic location	Hospital	5
Strategic location	CBD	5
Strategic location	Education (EDU)	5
Strategic location	University (UNI)	5

2.3.6 Network redundancy

Pipe redundancy plays a significant role in pipe replacement prioritisation. Pipe redundancy is calculated as follows:

The system is first balanced at the typical present operational average day demand scenario. Then a special routine evaluates the effect of the failure of every pipe individually. If the effect is that part of the network will not be supplied with water then the actual flow of the pipe is stored as criteria for the redundancy parameter. If the effect is that no part of the network will be isolated of water supply, then a value of zero is stored.

This analysis has been performed for Stellenbosch.

The following classification index was developed to rate this factor and shows the amount of flow that could not be delivered by the pipe if there is no redundancy.

Property	Criteria	Rating (0..5)
Redundancy (l/s)	0	0.1
Redundancy (l/s)	5	1
Redundancy (l/s)	10	2
Redundancy (l/s)	20	3
Redundancy (l/s)	50	4
Redundancy (l/s)	>50	5

2.3.7 Pavement management system (PMS)

As part of the PMS, roads are identified which should be upgraded by either resurfacing or reconstruction. This provides an independent assessment by an engineer of those roads that should be upgraded in the road network based on the assessment made for the PMS.

The rationale of the PMS item concept is that if a pipe has to be replaced due to likelihood of failure results, the replacement of this pipe can be brought forward if the PMS suggests future upgrading of the road within which the pipe falls.

The following classification index could be adopted in future to rate this factor:

Consequence of failure property	Criteria (<=)	Rating (0..5)
Pavement management system	(undefined)*	1
Pavement management system	Very good (VG)*	1
Pavement management system	Good (G)*	2
Pavement management system	Fair (F)*	3
Pavement management system	Poor (P)*	4
Pavement management system	Very poor (VP)*	5

* Data not available for or relevant to Stellenbosch Municipality

2.4 SOFTWARE MODEL

The *Wadiso® (GLS Software)* software has been extended to perform the required analysis. Results are then reported in the embedded GIS system per pipe and can be inspected in table or graphical format. Figure 1 shows on an aerial background image how the PRP score (as categorized in the legend) is also influenced by the slope analysis. Figure 2 shows a detailed graphical view of the same area.

It can for example be seen how the pipe highlighted in red has a number of LF and CF factors (including the location on the lower side of the road and high dynamic pressure) contributing to a relative high PRP score of 0.27. The short pipe shown in magenta has a PRP score of 0.30 mainly contributed also by its high FF and location under the tarred road.



Figure 1: Graphical result where PRP is also influenced by slope analysis (on aerial image)

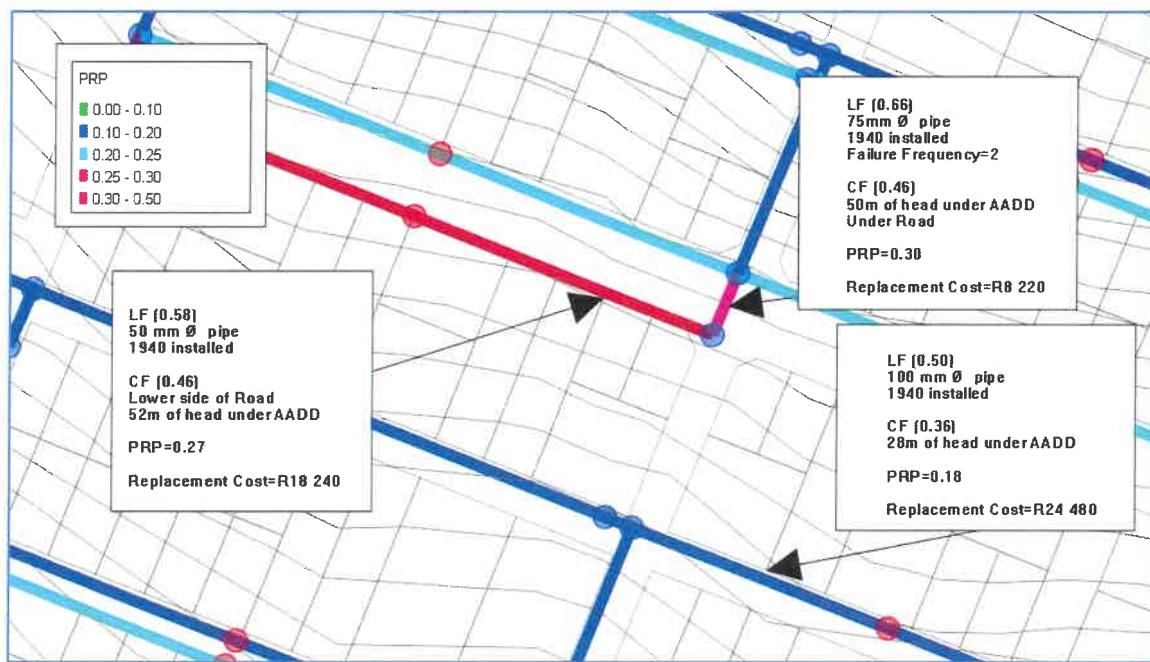


Figure 2: Graphical result – detail view

3. DISCUSSION OF RESULTS

The complete analysis has been performed for Stellenbosch Municipality. Results are available in the format of a GIS data set. The following is a discussion of results obtained and as presented in the included figures.

Figures SRW 1(a) to (e) show the total pipe replacement potential (PRP%) for each pipe in the model categorised as low (<60%), average (60%-80%), high (80%-90%) and very high (>90%). The higher the value, the higher the potential for replacement. Where a failure location is related to a pipe that has been replaced since the failure date, the location has been excluded from the map and deemed outdated.

The PRP per pipe was also rolled up per region (township/suburb/reservoir supply zone). Various options were investigated, such as a pipe length weighted average PRP per region. This identifies the areas where high PRP values are dominant and is shown in Figure SRW 2.

Table DRW 1 shows a list of pipes representing the top 112 pipes in Stellenbosch Municipality to be investigated for replacement, sorted in decreasing order of PRP together with their 2017/18 replacement value. Of these 112 pipes all 112 were identified as priority pipes where the PRP% of the pipe is > 85% and 3 or more incidents of pipe bursts were recorded on the pipe. These 112 priority pipes are also shown on Figures SRW 1(a) to (e) in blue together with their corresponding ranking, and a replacement value of R 8 591 220.

Table SRW 2 shows the total pipe failure record.

4. RECOMMENDATION

It was found that a number of pipe failures recorded by the field staff were not possible to be located. In these cases no address or only a street name without a street number was available. This should be brought to the attention of the field staff.

The location of pipe failures should in future be recorded preferably with accurate GPS coordinates. This would improve the integrity of the output of this pipe failure model. If a longer and more comprehensive pipe failure record could be established, the integrity of the output could be further enhanced.

It is recommended that pipe replacement in Stellenbosch Municipality is performed in accordance with the PRP values calculated in this study. Pipes with the highest PRP values should be considered to be replaced first. It should be noted that the priority pipes for replacement have been ranked only according to the criteria adopted for this study. The decision to replace a particular pipe or section of pipes should still however be taken on an engineering judgement basis using the results of this study as a guideline.

5. CONCLUSION

This new calibrated and tested pipe failure model identifies with a single geographical view where pipe failures are most likely to occur. It is foreseen that this model will greatly assist the pipe replacement prioritisation process as it is completely based on a scientific approach. By allocating funds to replacing those pipes most likely to fail in future, a limited budget can be spent effectively.

APPENDIX – FIGURES AND TABLES

Table SRW1: Top 150 pipes in Stellenbosch, Stellenbosch Municipality to be

PRP Rank	Model Link Nr	SYS TYP	SYSTEM	REGION	Diam (mm)	Length (m)	Fi (I)	Final LF	Final LF%	Final CF	Final CF%	Final PRP	Final PRP%	Repl Cost (R)	Cum Repl Cost (R)
79	8087	RET	Kleinvallei PRV 2	Stellenbosch	100	175	€ 3.6460	98.49	2.1460	27.41	7.8243	94.06	70 700	4 692 950	
80	13676	RET	Cloetesville reservoir	Stellenbosch	225	150	€ 3.5560	97.90	2.2000	47.29	7.8233	94.03	146 550	4 839 500	
81	13025	RET	Cloetesville reservoir	Stellenbosch	225	160	€ 3.5560	97.90	2.2000	47.29	7.8233	94.03	156 320	4 995 820	
82	19997	RET	Central	Stellenbosch	100	60	€ 3.6400	98.37	2.1460	27.41	7.8114	94.00	24 240	5 020 060	
83	16073	RET	La Coline PRV	Stellenbosch	150	35	€ 3.5320	97.85	2.2000	47.29	7.7705	93.76	19 530	5 039 590	
84	16757	RET	Central	Stellenbosch	100	160	€ 3.5140	97.75	2.2000	47.29	7.7309	93.51	64 640	5 104 230	
85	8252	RET	Kleinvallei PRV 2	Stellenbosch	100	215	€ 3.5940	98.11	2.1460	27.41	7.7127	93.45	86 860	5 191 090	
86	11354	RET	Papegaaiberg	Stellenbosch	100	150	€ 3.5940	98.11	2.1460	27.41	7.7127	93.45	60 600	5 251 690	
87	12575	RET	Welgelegen PRV	Stellenbosch	100	160	€ 3.5940	98.11	2.1460	27.41	7.7127	93.45	64 640	5 316 330	
88	13646	RET	Cloetesville reservoir	Stellenbosch	150	210	€ 3.4120	97.31	2.2541	57.00	7.6909	93.35	117 180	5 433 510	
89	11891	RET	Jamestown	Stellenbosch	75	220	€ 3.5760	97.98	2.1460	27.41	7.6741	93.16	88 880	5 522 390	
90	19982	RET	Uniepark 1	Stellenbosch	100	380	€ 3.4680	97.61	2.2000	47.29	7.6297	92.92	153 520	5 675 910	
91	15455	RET	Papegaaiberg	Stellenbosch	75	165	€ 3.5240	97.84	2.1460	27.41	7.5625	92.66	66 660	5 742 570	
92	15104	RET	Papegaaiberg	Stellenbosch	150	125	€ 3.4860	97.72	2.1460	27.41	7.4810	92.07	69 750	5 812 320	
93	8426	RET	Kleinvallei PRV 1	Stellenbosch	150	380	€ 3.4860	97.72	2.1460	27.41	7.4810	92.07	212 040	6 024 360	
94	12047	RET	Welgelegen PRV	Stellenbosch	100	175	€ 3.4680	97.61	2.1460	27.41	7.4423	91.61	70 700	6 095 060	
95	8072	RET	Kleinvallei PRV 2	Stellenbosch	100	280	€ 3.4680	97.61	2.1460	27.41	7.4423	91.61	113 120	6 208 180	
96	19967	RET	Central	Stellenbosch	100	245	€ 3.4620	97.47	2.1460	27.41	7.4295	91.53	98 980	6 307 160	
97	14657	RET	Cloetesville reservoir	Stellenbosch	150	200	€ 3.3600	97.18	2.2000	47.29	7.3921	91.43	111 600	6 418 760	
98	15311	RET	La Coline PRV	Stellenbosch	150	155	€ 3.3540	97.12	2.2000	47.29	7.3789	91.32	86 490	6 505 250	
99	40045	RET	Franschhoek - Wemmershoek re: Greater Franschhoek	Greater Franschhoek	100	70	€ 3.3960	97.24	2.1460	27.41	7.2878	90.19	28 280	6 533 530	
100	19877	RET	Uniepark 1	Stellenbosch	150	330	€ 3.2280	96.74	2.2541	57.00	7.2761	90.15	184 140	6 717 670	
101	19442	RET	Central	Stellenbosch	100	350	€ 3.2840	96.83	2.2000	47.29	7.2249	89.57	141 400	6 859 070	
102	9440	RET	Papegaaiberg	Stellenbosch	150	295	€ 3.3600	97.18	2.1460	27.41	7.2106	89.27	164 610	7 023 680	
103	14165	RET	Papegaaiberg	Stellenbosch	150	230	€ 2.9520	87.17	2.4407	84.14	7.2051	89.24	128 340	7 152 020	
104	12341	RET	Papegaaiberg	Stellenbosch	150	165	€ 3.3080	96.94	2.1460	27.41	7.0990	88.23	92 070	7 244 090	
105	8330	RET	Kleinvallei PRV 2	Stellenbosch	150	225	€ 3.3080	96.94	2.1460	27.41	7.0990	88.23	125 550	7 369 640	
106	11843	RET	Papegaaiberg	Stellenbosch	150	145	€ 3.3080	96.94	2.1460	27.41	7.0990	88.23	80 910	7 450 550	
107	10904	RET	Jamestown	Stellenbosch	75	560	€ 3.2200	96.70	2.2000	47.29	7.0841	87.53	226 240	7 676 790	
108	20171	RET	Uniepark 1	Stellenbosch	75	310	€ 3.2200	96.70	2.2000	47.29	7.0841	87.53	125 240	7 802 030	
109	20066	RET	Uniepark 1	Stellenbosch	150	385	€ 3.2040	96.47	2.2000	47.29	7.0489	86.97	214 830	8 016 860	
110	12677	RET	Central	Stellenbosch	110	250	€ 2.9052	82.93	2.4154	83.37	7.0173	86.57	101 000	8 117 860	
111	19583	RET	Central	Stellenbosch	315	320	€ 2.6380	61.63	2.6569	91.25	7.0088	86.19	432 960	8 550 820	
112	14609	RET	Cloetesville reservoir	Stellenbosch	110	100	€ 3.2540	96.77	2.1460	27.41	6.9831	85.84	40 400	8 591 220	

Stellenbosch	Alexander Bergzicht	14648	3.12/09/2014	2014	H/W/P				100 AC	899	
Stellenbosch	Holme-er t	14042	3.09/17/2014	2014	H/W/P				100 AC	899	1990
Stellenbosch	S libertas	18866	3.28/01/2014	2014	H/W/P				100 AC	899	1990
Stellenbosch	Centenburg	20192	1.04/05/2014	2014	H/W/P				75 AC	899	1965
Stellenbosch	19037	3.18/05/2014	2014	H/W/P				75 AC	899	1940	
Stellenbosch	34.Die land	18536	1.14/17/2014	2014	H/W/P				75 AC	899	1990
Stellenbosch	Hofmeyer st	18866	3.27/09/2014	2014	H/W/P				100 AC	899	1990
Stellenbosch	Neethling	17477	3.24/08/2014	2014	H/W/P				150 AC	899	1990
Stellenbosch	10.Vrede	15701	1.30/07/2014	2014	H/W/P				75 AC	899	1940
Stellenbosch	Vredie/Riet	16052	2.22/08/2014	2014	H/W/P				150 AC	899	1940
Stellenbosch	Vredie/Strand	15701	2.07/09/2014	2014	H/W/P				75 AC	899	1940
Stellenbosch	Aan de Wagen	13082	3.08/04/2014	2014	H/W/P				150 AC	899	1940
Stellenbosch	Papegaai str	13178	3.20/05/2014	2014	H/W/P				50 AC	899	1940
Stellenbosch	Piereleie/Vrede	16052	2.24/06/2014	2014	H/W/P				150 AC	899	1940
Stellenbosch	Skone uitsig	14441	3.15/10/2014	2014	H/W/P				150 AC	899	1940
Stellenbosch	Doornbosch	13976	3.27/11/2014	2014	H/W/P				150 AC	899	1940
Stellenbosch	Bird/Alexander	15284	2.22/06/2014	2014	H/W/P				100 AC	899	1990
Stellenbosch	Suidwai	15104	3.20/09/2014	2014	H/W/P				150 AC	899	1940
Stellenbosch	Piet Rietief	16052	2.07/09/2014	2014	H/W/P				150 AC	899	1940

Pipe Replacement Potential

— Low (<60%)

— Average (60%-80%)

— High (80%-90%)

— Very High (90%-100%)

— Priority pipes

● Recorded burst near unplaced pipe



Scale 1:50000



June 2019

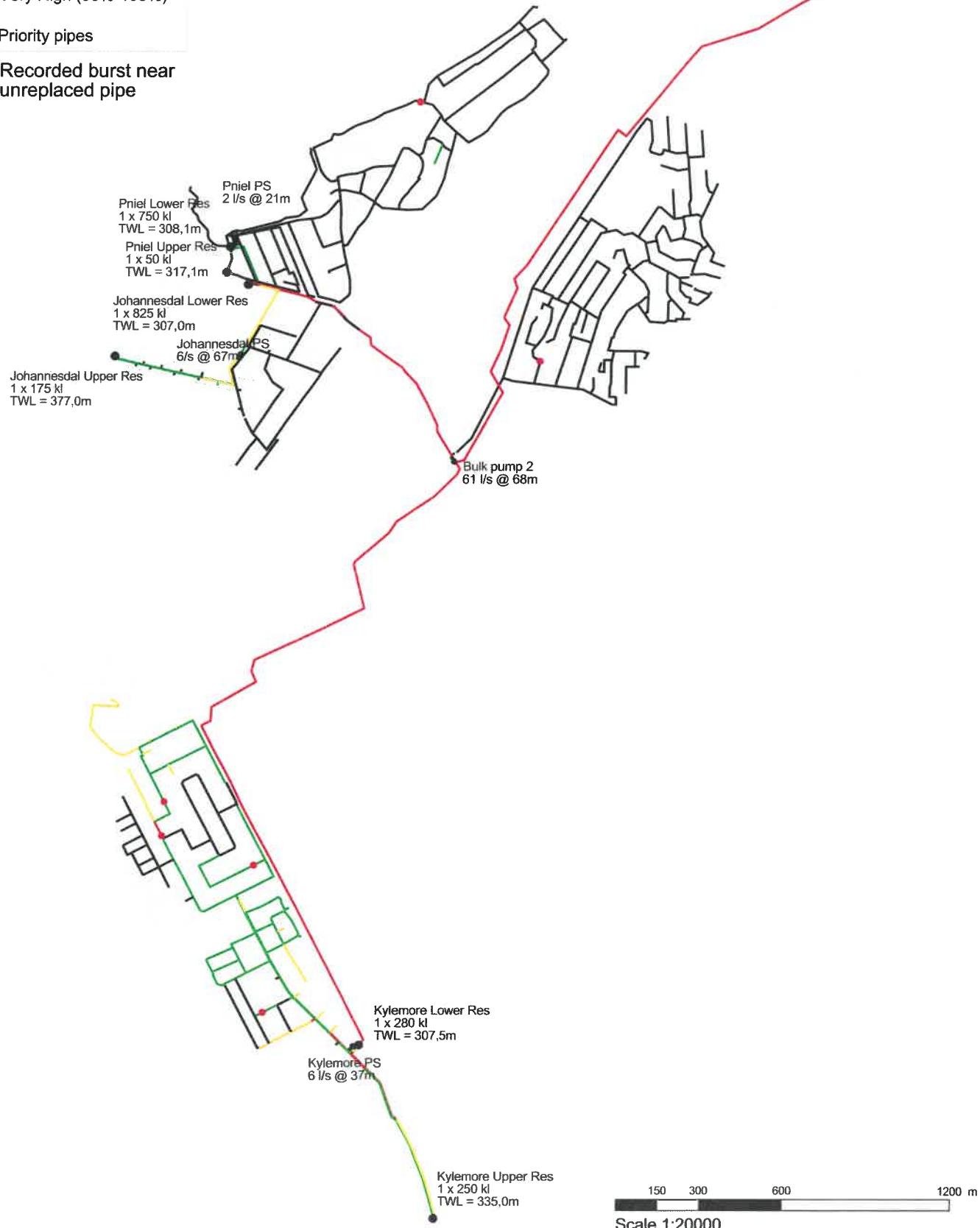
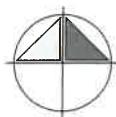
Pipe replacement study Stellenbosch



Figure SRW 1 (a)

Pipe replacement potential for
Stellenbosch

- Pipe Replacement Potential
- Low (<60%)
 - Average (60%-80%)
 - High (80%-90%)
 - Very High (90%-100%)
 - Priority pipes
 - Recorded burst near unreplace pipe



June 2019

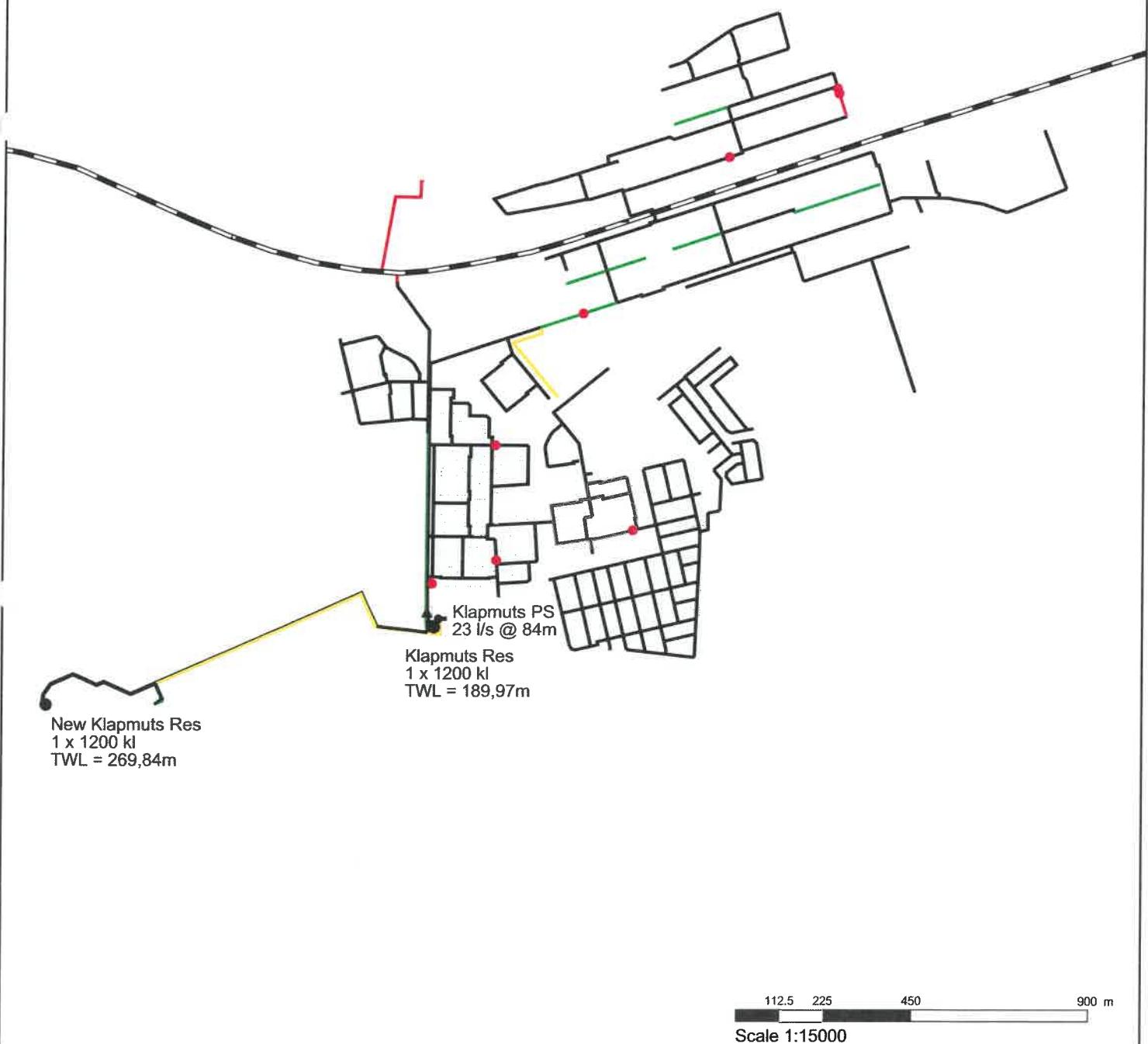
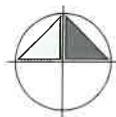
Pipe replacement study Stellenbosch



Figure SRW 1 (b)

Pipe replacement potential for Dwars River

- Pipe Replacement Potential
- Low (<60%)
 - Average (60%-80%)
 - High (80%-90%)
 - Very High (90%-100%)
 - Priority pipes
 - Recorded burst near unplaced pipe



June 2019

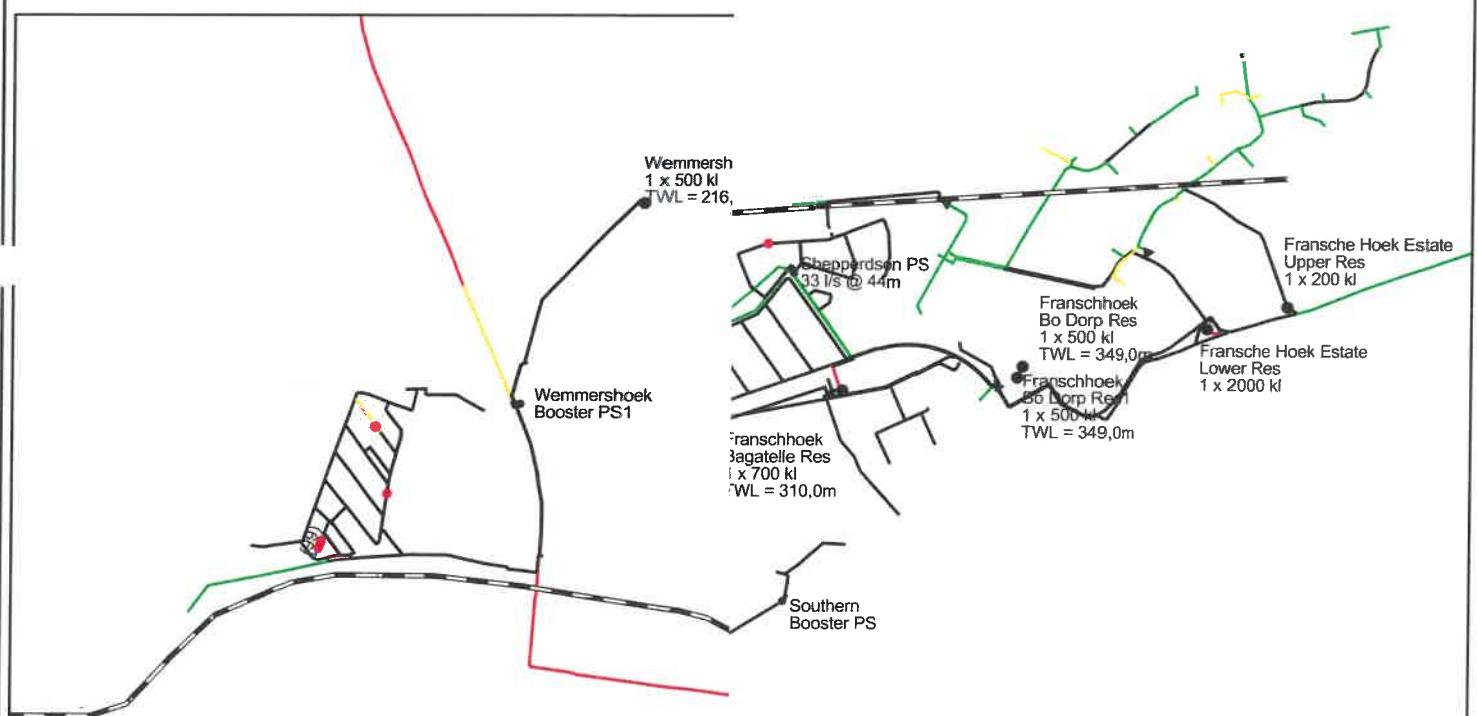
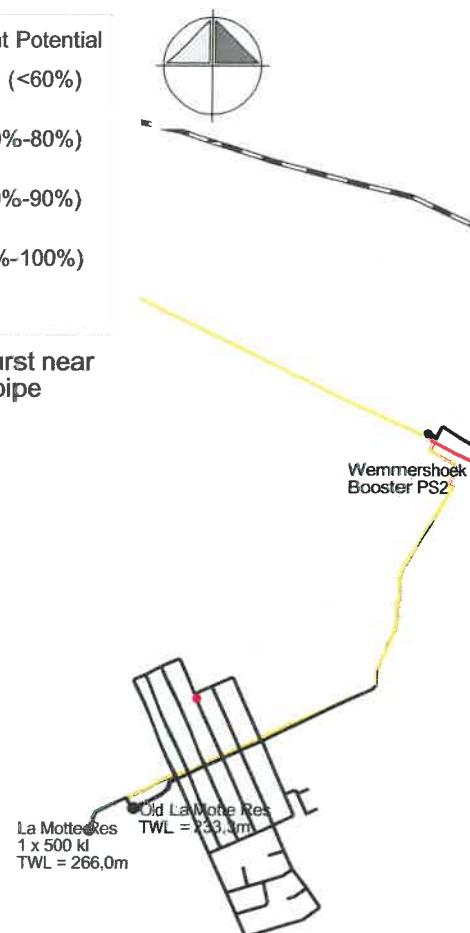
Pipe replacement study Stellenbosch

Figure SRW 1 (c)

Pipe replacement potential for Klapmuts

Pipe Replacement Potential

- Low (<60%)
- Average (60%-80%)
- High (80%-90%)
- Very High (90%-100%)
- Priority pipes
- Recorded burst near unreplaced pipe



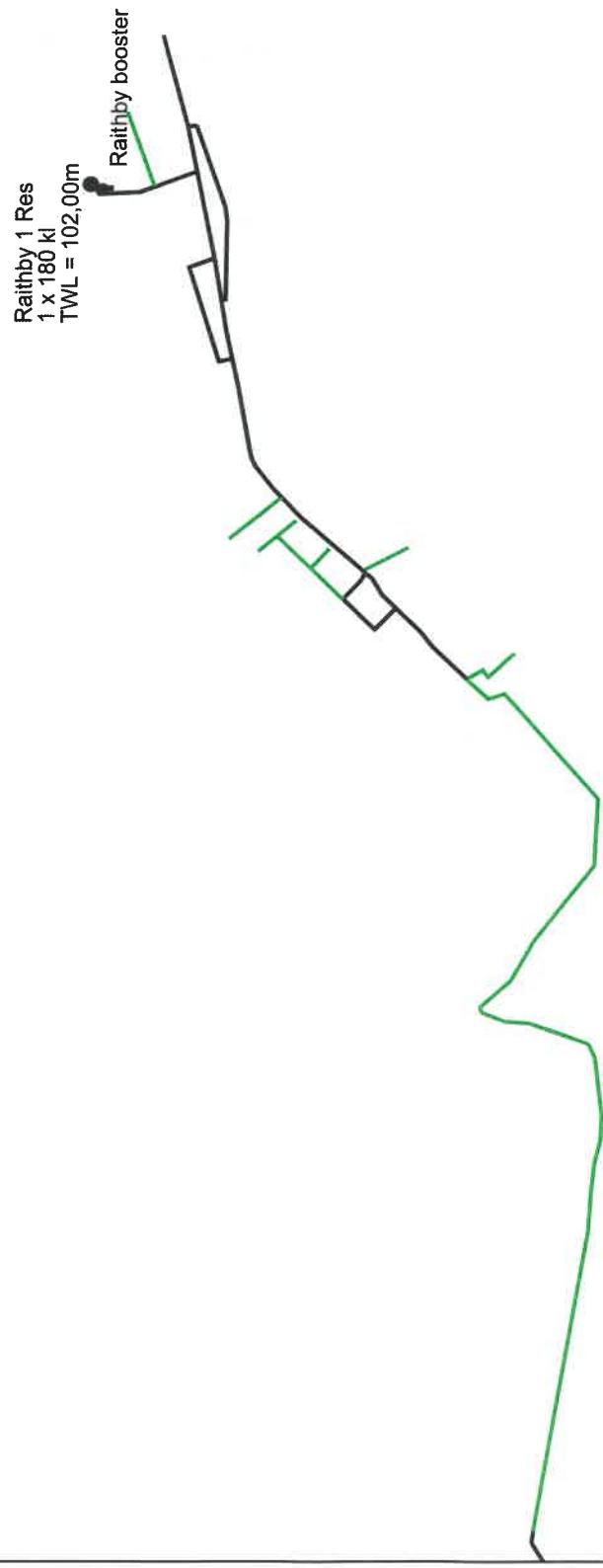
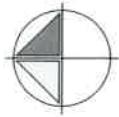
June 2019

Pipe replacement study Stellenbosch



Figure SRW 1 (d)

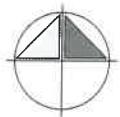
Pipe replacement potential for Franschhoek



June 2019
Pipe replacement study Stellenbosch

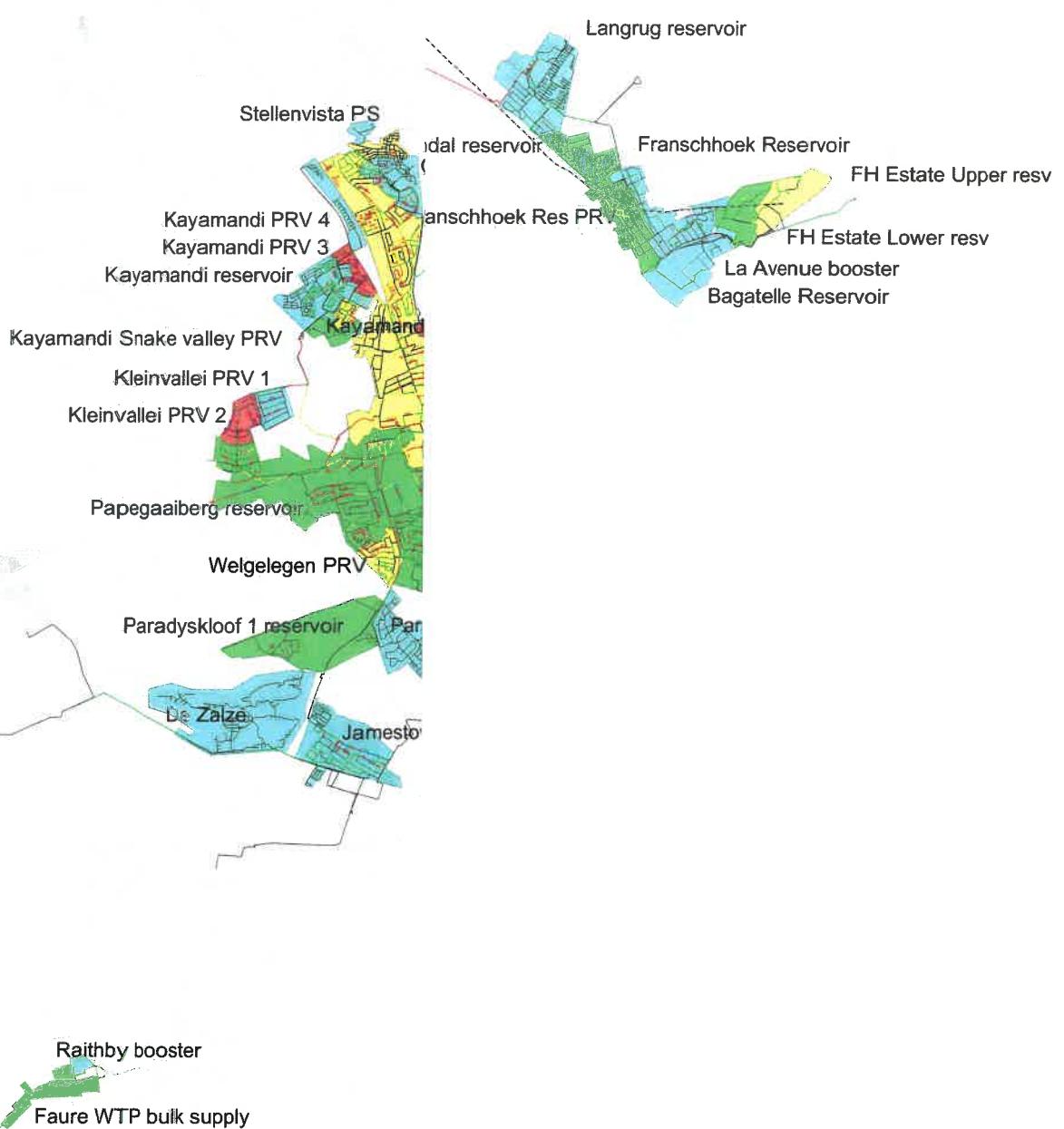


Figure SRW 1 (e)
Pipe replacement potential for
Raithby



Avg PRP(%)

- <60 %
- 60% - 80%
- 80% - 90%
- 90% - 100%



June 2019

Pipe replacement study Stellenbosch



Figure SRW 2

Pipe length weighted average PRP per Region (%)

LF weights				
Property	Weight	MaxRULDel	RULZeroPos	RULMode
L_NomDiam	5.4	25	3	1
L_ResPR	2.6	25	3	1
L_CRUL	4.6	25	3	1
L_MPItem	1.4	25	3	1
L_FailFreq	8.9	25	3	1
L_Material	7.1	25	3	1
L_Conditn	5	25	3	1

CF Weights	
Property	Weight
C_ConLossH	2.2
C_ConLossQ	2.2
C_RepCost	3.5
C_RoadSlpe	7.3
C_StratLoc	6
C_NWRedund	7.3
C_PMS	0

LF Legend				
Property	Criteria	Rating	Count	CountP
L_NomDiam	0.001	2.5	0	0.0
L_NomDiam	50	5.0	309	4.4
L_NomDiam	76	4.0	639	9.0
L_NomDiam	98.9	3.0	69	1.0
L_NomDiam	99	2.5	252	3.6
L_NomDiam	110	3.0	2697	38.2
L_NomDiam	160	2.0	1587	22.5
L_NomDiam	250	1.0	961	13.6
L_NomDiam	400	0.5	474	6.7
L_NomDiam	10000	0.1	73	1.0
L_ResPR	0.0	0.1	287	4.1
L_ResPR	0.25	1.0	641	9.1
L_ResPR	0.5	2.0	2006	28.4
L_ResPR	0.75	3.0	2242	31.8
L_ResPR	0.999	4.0	1697	24.0
L_ResPR	10000	5.0	188	2.7
L_CRUL	-100	5.0	0	0.0
L_CRUL	0	5.0	1934	27.4
L_CRUL	10	4.0	1837	26.0
L_CRUL	20	3.0	1086	15.4
L_CRUL	30	2.0	396	5.6
L_CRUL	50	1.0	832	11.8
L_CRUL	10000	0.1	976	13.8
L_MPItem		3.0	7061	100.0
L_MPItem	FS	3.0	0	0.0
L_MPItem	MP	5.0	0	0.0
L_FailFreq	0.00	0.1	6508	92.2
L_FailFreq	1	0.5	121	1.7
L_FailFreq	2	1.0	163	2.3
L_FailFreq	3	3.0	87	1.2
L_FailFreq	4	4.0	48	0.7
L_FailFreq	10000	5.0	134	1.9
L_Material	AC	5.0	2897	41.0
L_Material	CI	3.0	13	0.2
L_Material	COPPER	5.0	0	0.0
L_Material	DI	1.0	2	0.0
L_Material	FC	5.0	0	0.0
L_Material	GRP	1.0	0	0.0
L_Material	HDPE	1.0	229	3.2
L_Material	LDPE	2.0	0	0.0
L_Material	MPVC	2.0	0	0.0
L_Material	OPVC	2.0	0	0.0
L_Material	PVC	2.0	402	5.7
L_Material	POLY	4.0	0	0.0
L_Material	STEEL	1.0	284	4.0
L_Material	SS	1.0	0	0.0
L_Material	UNK	3.0	1490	21.1
L_Material	UPVC	2.0	2028	28.72114431
L_Material	ST	1.0	0	0.0
L_Material	CU	5.0	0	0.0
L_Conditn		3.0	7056	99.9
L_Conditn	F	3.0	0	0
L_Conditn	G	2.0	0	0
L_Conditn	P	4.0	3	0.0424869
L_Conditn	VG	1.0	0	0
L_Conditn	VP	5.0	2	0.0283246

CF Legend				
Property	Criteria	Rating	Count	CountP
C_ConLossH	0	0.1	265	3.8
C_ConLossH	25	1.0	685	9.7
C_ConLossH	50	2.0	2298	32.5
C_ConLossH	75	3.0	2845	40.3
C_ConLossH	100	4.0	875	12.4
C_ConLossH	10000	5.0	93	1.3
C_ConLossQ	0	0.1	174	2.5
C_ConLossQ	5	1.0	5975	84.6
C_ConLossQ	10	2.0	201	2.8
C_ConLossQ	20	3.0	191	2.7
C_ConLossQ	50	4.0	117	1.7
C_ConLossQ	10000	5.0	403	5.7
C_RepCost	0	1.0	539	7.6
C_RepCost	1	1.0	6522	92.4
C_RepCost	2	3.0	0	0.0
C_RepCost	3	5.0	0	0.0
C_RoadSlpe		3.0	7055	99.9
C_RoadSlpe	MIDBLOCK	5.0	6	0.1
C_StratLoc		3.0	6407	90.7
C_StratLoc	CBD	4.0	146	2.1
C_StratLoc	EDU	5.0	78	1.1
C_StratLoc	HOS	5.0	19	0.3
C_StratLoc	IND	5.0	102	1.4
C_StratLoc	UNI	5.0	309	4.4
C_NWRedund	0	0.1	4211	59.6
C_NWRedund	5	1.0	2185	30.9
C_NWRedund	10	2.0	102	1.4
C_NWRedund	20	3.0	86	1.2
C_NWRedund	50	4.0	91	1.3
C_NWRedund	10000	5.0	386	5.5
C_PMS		1.0	7061	100.0
C_PMS	F	3.0	0	0.0
C_PMS	G	2.0	0	0.0
C_PMS	P	4.0	0	0.0
C_PMS	VG	1.0	0	0.0
C_PMS	VP	5.0	0	0.0

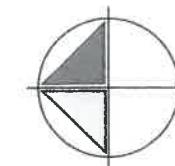


June 2019



Pipe replacement study Stellenbosch

Pipe Replacement Potential	
—	Low (<60%)
—	Average (60%-80%)
—	High (80%-90%)
—	Very High (90%-100%)
—	Priority pipes (numbered)



- Recorded burst near unreplaced pipe

